

Assessment of Depression Impact on Runoff Characteristics Using GIS Technique

Morad Abdelsalheen, Ashraf M. Elmoustafa, Ahmed A. A. Hassan

Abstract— Depression is a storage volume that could be filled prior to runoff. It might be used as a rectification parameter to adjust runoff volumes and peak discharges. GIS tools are used to extract depressions and calculate their characteristics (volume – area) and to pick the corresponding catchments and estimate their characteristics from DEM. In this work, HEC-HMS is used as a step to calculate runoff using three approaches to assess the impact of presence of depressions on runoff from three points of view; outlet location, runoff volume and peak discharge downstream the depression. First approach neglects the presence of depression. Second approach accounts depression in study but assuming one outlet with width equal to one cell size and lastly the third approach is as same as second approach but multi outlets are used with different widths and levels. The last approach gives more realistic value for runoff volume and peak discharge as it accounts volume of water stored in depression and represents the outflow from depression in an accurate way.

Index Terms — GIS, Depression, HEC-HMS, Routing, Runoff.

I. INTRODUCTION

Rainfall and runoff processes can be studied either by physical or numerical model [1]. Runoff passing through a reservoir is attenuated as it can be temporarily stored during storms in the reservoir or depression to mitigate downstream flooding. The continuity and momentum equations are applied to investigate runoff propagation through a reservoir [2]. Furthermore, Routing techniques are used to deduce surface runoff hydrographs. Selection of runoff routing method is effective as it related to the nature of Up-stream watershed characteristics and required accuracy. Also, routing is classified as hydrologic and hydraulic. For Hydrologic models, they have a closed form of solution equation, while hydraulic models need numerical integration with a finite difference approach [3]. HEC-HMS is used for calculating the runoff volume and peak discharge resulting from catchments and reservoirs using different techniques of hydrological modeling and routing.

II. METHODOLOGY

In the present study, a Hydrologic Modeling System (HEC-HMS) was used to calculate runoff volumes and peak discharges by simulating the precipitation – runoff processes

of drainage catchments through applying the Soil Conservation Service SCS methodology equations. While the attenuation caused by depressions was simulated through applying Outflow structures routing by presenting the depression as a reservoir and its outlet as long-crested spillway.

Reservoir within HEC-HMS are not simulated to receive precipitation so a pseudo sub-basin with the same top surface area of depression is used to simulate direct rainfall into depression (lag time = minimum)[4]. And the outflow from retention with horizontal water surface can be computed with level-pool routing which discretizes time into equal intervals of duration (Δt). one-dimensional approximation of continuity equation can be used to simulate routing.

$$I_{avg} - O_{avg} = \frac{\Delta S}{\Delta t} \quad (1)$$

Where, I_{avg} and O_{avg} are average inflow and outflow during time interval; ΔS is storage change during the same duration, with finite difference approximation, equation (1) can be written as:

$$\frac{I_t + I_{t+1}}{2} - \frac{O_t + O_{t+1}}{2} = \frac{S_{t+1} - S_t}{\Delta t} \quad (2)$$

Where, t is index of time interval; I_t and I_{t+1} are inflow values at the beginning and end of the t^{th} time interval respectively; and O_t and O_{t+1} are corresponding outflow values; and S_t and S_{t+1} are corresponding storage values[5].

Outflow structures routing method is used in this model, as it accounts for reservoirs with number of uncontrolled outlet structures. Automatic adaption of time step selection method was used to get possible precision in the results[6]. Outlets were chosen as spillway to simulate overflow of water from depression and a long-crested spillway is selected as a type of spillway.

In Equation 4, for long crested weir, by increasing crest length coefficient of weir decrease[7]. Thus, C was taken with a minimum value (1.10) from the recommended HEC-HMS range (1.10 to 1.66).

$$Q = C * B * (H)^{2/3} \quad (3)$$

$$C = 3 \left(\frac{H}{L} \right)^{0.022} \quad (4)$$

In this study, three approaches were used to evaluate the effect of depression geometry and outlet characteristics on runoff volume and peak discharge. In first approach, catchments were defined by intersecting between drainage lines and outer perimeter of depression but depression was treated as a catchment area, Figure 1. Likewise, in second and third approaches, the corresponding catchments were calculated as same as first approach. Table 1 Illustrates catchments' morphological parameters for different approaches.

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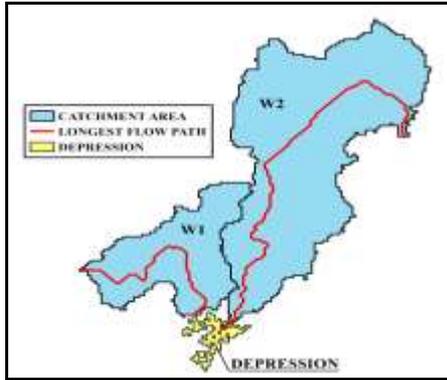


Figure 1 Catchments Definition

Table 1 Catchments' Morphological Parameters

Catchment Name	Catchment Area (Km ²)	Longest flow path (m)	CN assumed	T _C (min)	T _{Lag} (min)
W1	16.52	8308	75	396	238
W2	46.02	17261	75	606	364
DEPRESSION	1.57	2485	75	202	121

A. First Approach

In this approach, as most of morphological models incorrectly do. Runoff generated from catchments was calculated assuming no depression effect was considered. The total depression surface area was considered and treated as a catchment area free from depressions and a semi-distributed model (HEC-HMS) was used to calculate runoff volume and peak discharge at an outlet point (junction) downstream the depression. In this approach, assuming the Drainage lines will continue in their direction. Peak discharge and runoff volume were calculated at a collection point (junction) downstream the depression accounting the corresponding catchments and also depression area as a catchment. Figure 2 .

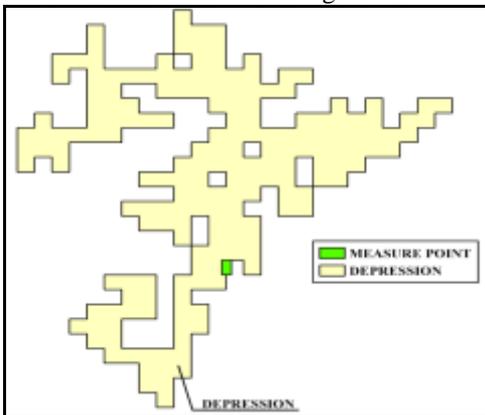


Figure 2 Peak Discharge and Runoff Volume Measuring Locations (1st Approach)

However, in second and third approaches, the outlet were defined as lowest point/points in the depression perimeter.

B. Second Approach

In this approach, the depression effect was considered, the runoff from catchments and intercepted precipitation by depression were used to fill out depression volume then overflowed from one outlet (lowest one) which is the outlet point considered in the first approach. HEC-HMS was also used to calculate runoff volume and peak discharge of excess flow from depression assuming the outlet as one long-crested spillway with crest width equal to one cell size. The outlet location was defined as a spillway with crest width equal to

one cell size. Which was located at one of lowest parts of depression perimeter. Figure 3

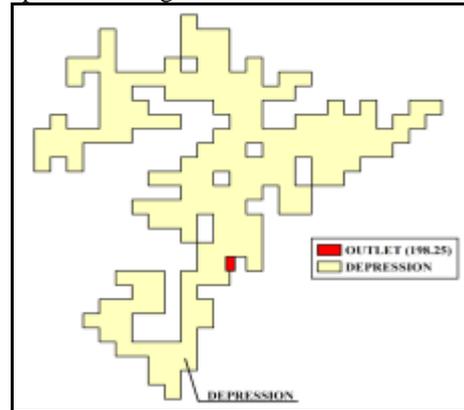


Figure 3 Outlet Location in 2nd Approach

C. Third Approach

Similarly, in this approach, the depression effect was also considered yet using a more realistic simulation of outlet points. The runoff from catchments and intercepted precipitation by depression were used to fill out the depression volume then overflowed from multi outlets (lowest points along the perimeter). HEC-HMS was also used to calculate runoff volume and peak discharge of excess flow from depression assuming the outlets as long-crested spillways with different crest widths and levels. The outlets locations were defined as a multilabel spillways with different crest widths and levels. Which were located at the lowest parts of depression perimeter. Figure 4.

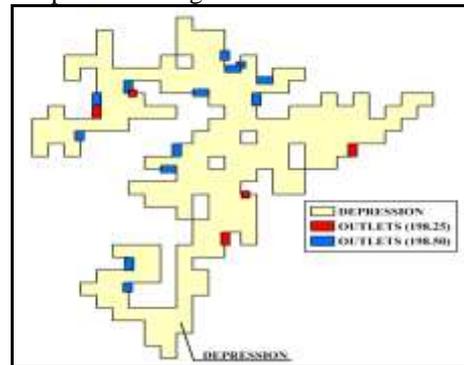


Figure 4 Outlets Locations in 3rd Approach

III. DEPRESSION MORPHOLOGICAL CHARACTERISTICS

A. Perimeter Profile

Using ARC-GIS, extracting crest widths and levels is accomplished by defining depression first, then generating a profile for the depression perimeter, Figure 5, Finally grouping crests with same level. Table 2 shows the crest width at each level of outer perimeter of depression.

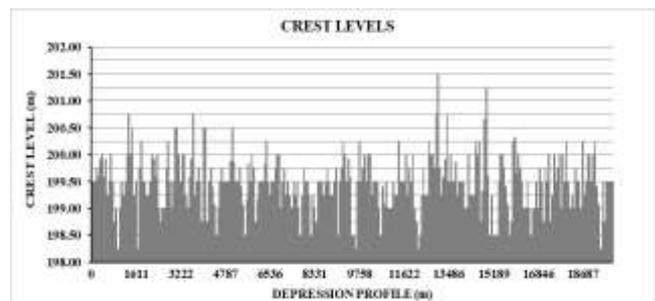


Figure 5 Depression Perimeter Profile

Table 2 Length at each level of Outer perimeter of Depression

Elevation (m)	Length (m)
198.25	368
198.50	1066
198.75	852
199.00	1995
199.25	2470
199.50	5224
199.75	1757
200.00	2186
200.25	805
200.50	483
200.75	245
201.00	0
201.25	69
201.50	92
Total Length	17612 m

B. Volume Rating Curve and Surface Area

Figure 6 was also developed using GIS tools which show Volume Rating Curve and Surface Area for the depression at each level. The morphological parameter for depression can be summarized as follow:

- Total Length of Outer Perimeter = 17,612 m.
- Top Surface Area = 1,567,745 m²
- Total Volume = 4,732,894 m³

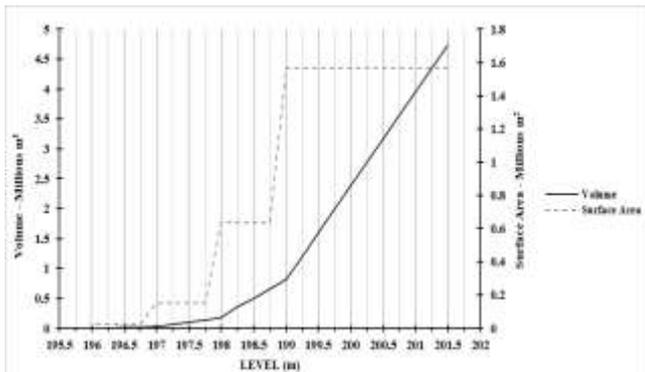


Figure 6 Volume Rating Curve and Surface area for Depression

IV. STORM DESCRIPTION

A hypothetical storm was used in the study with a depth of 150 mm which was applied as a uniform storm on the area of the depression and its corresponding catchments. This value was selected by trials in order to operate multi spillways with different crest heights. A Soil Conservation service (SCS-II) storm method implemented as a design storm pattern which was applied on all sub-basins (catchments /depression).

V. RESULTS

A. Runoff Volume

To evaluate the effect of depression (reservoirs), Storage Ratio (SR) was used which attained with dividing the stored volume by the total volume of inflow at the reservoir. Positively, the higher values of these indices are, the greater efficiency is of reservoirs in detention[8].

For second and third approaches, computed runoff volume composed of the volume of water calculated at outlets (Spillways) after subtracting the depression storage.

Conversely, for first approach the depression effect in neglected.

Table 3 Runoff Volumes for three approaches

Approach	Calculated Inflow volume (1000 m ³)	Calculated Outflow volume (1000 m ³)	Volume stored (1000 m ³)	SR (%)
First	5236.26	5236.26	0.00	--
Second		4869.40	366.86	7.00
Third		4868.40	367.86	7.03

In Table 3, It is obviously noted that for second and third approaches have almost the same percentage of (SR) with a minute difference about 0.03% between two approaches due to difference in outlets configurations (Spillways).

B. Peak Discharge

The values of peak discharge reduction depend on the level up to which a reservoir is filled[9]. In this study, depression was assumed to be empty before the storm. Flood Attenuation Ratio (FAR) is defined as the ratio of discharge reduction in the reservoir (difference between the maximum input and output discharges) to the input peak discharge in the reservoir[8]. And was used to compare between the three approaches.

Table 4 Peak Discharge for three approaches

Approach	Peak Inflow (m ³ /sec)	Peak Outflow (m ³ /sec)	Difference (m ³ /sec)	Peak water level (m)	FAR (%)
First	139.48	126.45	13.03	--	10.30
Second		139.04	0.44	198.62	0.32
Third		113.06	26.42	199.33	18.94

In Table 4, It is clearly seen that there is a great difference in FAR between second and third approaches and this was due to difference in outlets configuration (Spillways). Also, water was stored in second and third approaches to level 198.62m and 199.33m respectively. And this was a result for when a one outlet was used, water was stored to higher level until discharged. But for multi-outlets water was stored to level 0.71m lower than third approach. For the first approach, peak outflow was a middle value between first and second approaches not because of depression but due to longest flow path characteristics.

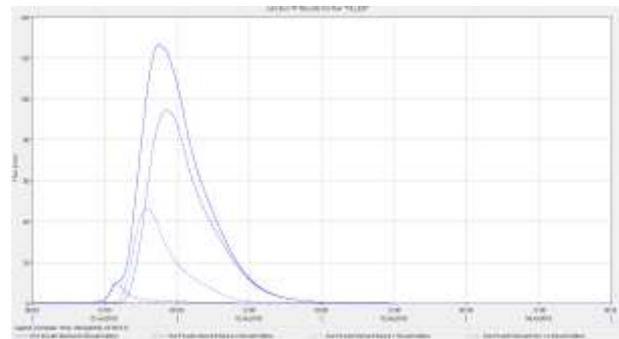


Figure 7 Storage, water elevation and flow versus time for 1st Approach

Figure 7 shows the runoff discharge from each catchment (W1, W2 and Depression as a catchment) and the cumulative discharge from all catchment. And maximum runoff discharge was 126.45 m³/sec.

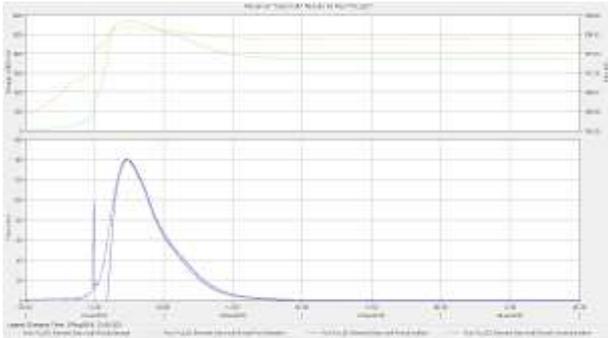


Figure 8 Storage, water elevation and flow versus time for 2nd Approach

For the second approach, *Figure 8* reveals two graphs. The first graph shows storage in 1000m³ and water level with time. And second graph also shows the peak discharge with time. The storage, water level and peak discharge were 367860 m³, 199.33m and 113.06 m³/sec respectively.

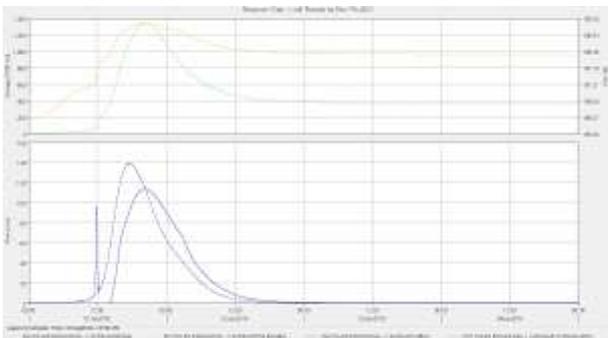


Figure 9 flow versus time for 3rd approach

Similarly, for the third approach, *Figure 9*, The storage, water level and peak discharge were 366860 m³, 198.62m and 139.04 m³/sec respectively.

VI. CONCLUSIONS

Outflow volume is depending on depression characteristics and doesn't affected with the configuration of spillway. and peak discharge affected with the configuration of spillway.

From the previous results, three approaches were conducted, the first one which most hydrological models adopt, assumes no depression exists. And this is inaccurate assumption in calculating runoff volume as it gets the highest value of outflow volume as no water stored in a depression. For the second approach, one outlet was used and it is also not a real approximation but it can be used as an approach in calculating outflow volume but not in a conservative way. In third approach, which is most real one, As when water fills the depression volume and start to flood out from depression, it floods from different outlets hence, the resulting water level in this approach is lower than second one and leading to the most conservative values of peak outflow. Also, it gives a non-conservative but more realistic value for runoff volume as a portion of water is stored in depression.

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