

Pattern Recognition of Pitch Motion for A New High Speed Gliding-hydrofoil Craft and Its Method

Gao Shasha, Yang Songlin, Liu Man, Shi Yan, Cao Zhiwei

Abstract— In this paper, a series of still water free decay experiments were carried out on a gliding-hydrofoil craft. By establishing the mathematical model of pitch motion mode, and based on system identification theory and genetic algorithm, the system identification software was written in C# language. (1) A mathematical model of 3 kinds of pitch motion was established. The pitch motion of three different drafts and different initial pitch angles were identified and calculated. The conclusion is that the fitting effect of the equation 1 is the best; (2) By calculating the angular velocity forecasting values for various operating conditions, the errors between the experimental values and the fitted values were analysed. It is found that the consistency of the forecast value and the test result is good, which proves the reliability of the system identification software; (3) Based on the identification results, the variation of each hydrodynamic torque coefficient with draft and initial pitch angle analysed. The analysis results and methods can provide a reference for sea-keeping research of such unmanned craft, and provide important technical support for subsequent optimization design of craft type.

Index Terms— gliding-hydrofoil craft; pitch motion mode; pitching attenuation test; pattern recognition

I. INTRODUCTION

In the course of craft navigation, due to the interference of sea waves, sea wind and other environmental factors, the craft will produce a total of 6 degrees of freedom, such as rolling, pitching, yawing, swaying, surging and heaving. For rolling motion, the purpose of anti-rolling can be achieved by means of stabilizer and other control methods. But for pitching motion, there is no effective way. Therefore, the study of pitch motion is an important research topic in the field of craft motion.

At present, researches on pitching motion are mainly carried out in two aspects. The first is the theoretical calculation.

Such as slicing theory and slender body theory, and so on, and the use of theoretical calculation, to calculate and predict the craft's swing motion in the wave; on the other hand, the motion law of craft's pitching motion in certain water environment is studied by means of experiment, such as model test and so on. Wang Zhidong and so on^[1] by using the software FLUENT of computational fluid dynamics, developed the coupled solution of the longitudinal motion prediction program of the gliding craft, and carried out the numerical simulation of the motion response of the three-dimensional gliding boat model in the uniform flow,

which provides an effective method for the real-time numerical prediction of the motion response of the gliding craft. According to the characteristics of the motion of high speed boats in still water and waves, a new method for predicting the longitudinal motion of high speed craft is proposed by Dong Wencai and other^[2] of the Naval Engineering University. This method can predict the longitudinal motion of the wave in the medium and high speed. However, this method is not suitable for predicting the longitudinal motion of high speed craft at low velocity. Liu Cheng^[3] proposed a support vector machine prediction model based on particle swarm optimization and grey model. The model has high prediction accuracy. In view of the grey characteristics of the craft's longitudinal motion system, Zhao Shuang and others^[4] studied the prediction problem of the nonlinear longitudinal motion of crafts in sea waves by using the topological prediction method and the GM (1,1) model. The study of the craft's longitudinal motion prediction using topological prediction model is reasonable and feasible. Winer and others^[5] used the method of statistical prediction to predict craft's pitch, and Triantafyllou^[6] used the Calman filter method to predict the craft's pitching.

For the theoretical study of the craft's longitudinal motion, although it can reach the purpose of the motion prediction, there are still many problems to be obtained by theoretical calculation only. The correctness and reliability of the results are not easily verified, and the results of the theoretical study are verified by experimental research.

We generally refer to the test methods, including full-scale test and model test. Full-scale test usually refers to using full-scale craft to carry out a test on a specific sea surface after the completion of a craft, and to obtain data or curves representing the characteristics of the craft's motion. This method is harsh to the environment and it's expensive. It is difficult for the average scientific research institutions or researchers to undertake such a cost. The practical feasibility is low. The craft model test refers to the method of making the corresponding craft model in accordance with a certain scale of shrinkage for a real ship, making the corresponding craft model in the standard pool to obtain the results of the craft test. This method is relatively less expensive and more feasible than the actual craft test. In general we compare the results of the theoretical calculation with the test results to verify each other. This method is used in this paper.

In this paper, the model of high speed gliding craft model was tested and analyzed. The system identification mathematical model and method^[7] based on genetic algorithm was established. The identification software was developed and the identification analysis of the pitch motion was carried out. By analyzing the identification results and test data, the feasibility of the model was verified, and the reliability of system identification was verified.

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II. SCHEME FOR PITCH TEST OF CRAFT MODEL

An optimized gliding craft model is selected for the pitching test. Its principle dimensions are shown in table I.

Table I. The main parameters of the optimized unmanned craft

Parameter	Symbol	value	Unit
Length	L	1.50	m
Width	B	0.46	m
Depth	D	0.18	m
Draft	T	0.11	m
Displacement	Δ	34.55	kg
Speed	V	8.00	kn

The experiment was carried out at the towing tank of Jiangsu University of Science and Technology. The towing tank is 100 meters long, 6 meters wide, and the largest depth of water is 2 meters. In this paper, the attenuation law of craft model was determined by measuring the variation of pitch angle in the free attenuation process of static water. Before the test, the weight of the craft and the position of the center of gravity were measured before-hand. The specific test process is as follows:

(1) We prepared for trial the instrument including test model with length of 1.5 meters, MTi-G inertial measuring instrument (six degrees of freedom motion of measurable craft), data transmission line and computer;

(2) The MTi-G inertial measurement unit was placed horizontally on the center of gravity of the craft's model and connected to the equipment with data lines;

(3) The craft model was placed in the center of the pool, and the craft model was adjusted by loading weights to make it at the state of zero trim;

(4) When the model was at the state of zero trim, the pitch angle of the craft model was read by MTi-G software. By adjusting the horizontal position of the MTi-G, the initial pitch angle of the software was guaranteed to be between 0.01 degrees;

(5) When craft model was stable, the external force was applied according to the angle marking symbol. While releasing the external force, the MTi-G measuring instrument was used to collect data and allow the craft model to freely pitching. When the model was stable again, the data acquisition was stopped;

(6) In the process of repeating (4) - (5), the initial angle of pitching was changed. The initial angle of pitching was five groups of designed draft, including 1, 2, 3, 4, 5 degrees. For each group, the initial pitch angle was tested for 2-3 times, and the best one was selected as the effective data;

(7) The design draft pitch test was carried out by adding or reducing ballast by 1.1 and 0.9 times, repeated steps (4) - (6).

III. SYSTEM IDENTIFICATION EQUATION AND MATHEMATICAL MODEL

The definition of Zadeh [8] is that identification is based on input and output data, and determines a model that is equivalent to the measured system from a given set of model classes. Generally speaking, there are three elements in identification: data, models and criteria. Identification is to select a model that best fits the data in a set of model classes according to a criterion.

1. Righting Moment

When the craft is pitching at a certain angle, the center of gravity and the center of buoyancy are not on the same vertical line, which produces a moment to return the craft to its original position. This is the righting moment. The initial stability formula is as follows:

$$M(\psi) = -DH\psi \quad (1)$$

Where, D is the displacement of the craft and H is the initial stability height.

2. Damping moment

Pitch damping is a function of angular velocity, which is generally expressed as:

$$M(\dot{\psi}) = -2N\dot{\psi} - W\left|\dot{\psi}\right|\dot{\psi} - x\dot{\psi}^3 \quad (2)$$

Where, N , W and x are pitching damping moment coefficients.

3. Inertia moment

There is angular acceleration in the course of rotation of crafts, and the moment of inertia must be generated. The inertia moment of the pitch is made up of two parts. This is the inertia moment and additional moment of inertia of the craft itself. Generally speaking, they are linearly related to angular acceleration:

$$M(\ddot{\psi}) = -(I_{yy} + J_{yy})\ddot{\psi} = -I_{yy}\ddot{\psi} \quad (3)$$

According to the dynamic balance principle of the body, the equilibrium condition of the craft model is $\sum M = 0$, and the equilibrium equation of the craft model in still water is:

$$M(\ddot{\psi}) + M(\dot{\psi}) + M(\psi) = 0 \quad (4)$$

Based on the above equilibrium equations, three equations of pitch motion have been established for system identification analysis, and the pitching equation of craft model has been found.

Equation 1:

$$-2N/I'_{yy}\dot{\psi} - W/I'_{yy}\left|\dot{\psi}\right|\dot{\psi} - x/I'_{yy}\dot{\psi}^3 + C_1/I'_{yy}\psi^3 + C_2/I'_{yy}\psi^2 + C_3/I'_{yy}\psi = 0$$

(5)

Equation 2:

$$-2N/I'_{yy}\dot{\psi} - W/I'_{yy}\left|\dot{\psi}\right|\dot{\psi} - x/I'_{yy}\dot{\psi}^3 + DH/I'_{yy}\sin\psi = 0 \quad (6)$$

Equation 3:

$$-(I_{yy} + J_{yy})\ddot{\psi} - 2N\dot{\psi} - W\left|\dot{\psi}\right|\dot{\psi} - x\dot{\psi}^3 + C_1\psi^3 + C_3\psi = 0 \quad (7)$$

Where, h is initial stability height; D represents the displacement; I'_{yy} represents the total inertia moment; ψ means the pitch angle; $\dot{\psi}$ represents the angular velocity of pitch; $\ddot{\psi}$ represents the angular acceleration of the pitch; $2N$ represents the coefficient of linear damping torque; W , x representation of nonlinear damping moment coefficient; C_1 , C_2 representation of nonlinear righting

moment coefficient; C_3 represents the coefficient of linear righting moment.

Taking equation 2 as an example, we discretized it and got the following formula.

$$\frac{(\psi_{k+1} - \psi_k)}{t} = -2 \frac{N_1}{I'_{yy}} \psi_k - \frac{W_1}{I'_{yy}} |\psi_k| \psi_k - \frac{x_1}{I'_{yy}} \psi_k^3 - \frac{DH_1}{I'_{yy}} \sin \psi_k \quad (8)$$

The prediction of the pitch angular velocity at the $k + 1$ moment is shown below.

$$\psi_{k+1} = (-2 \frac{N_1 t}{I'_{yy}} + 1) \psi_k - \frac{W_1 t}{I'_{yy}} |\psi_k| \psi_k - \frac{x_1 t}{I'_{yy}} \psi_k^3 - (\frac{DH_1 \sin \psi_k}{I'_{yy}}) t \quad (9)$$

By measuring the angle of the experimental K, there are error estimation criteria at K+1 time:

$$E_{K+1} = \psi_{K+1} - \psi_{K+1} \quad (10)$$

According to the error estimation criterion, the objective function of pitch identification model is established as follows:

$$F(x) = \sqrt{\frac{1}{N} \sum_{k=1}^N (\psi_{k+1} - \psi_{k+1})^2} \quad (11)$$

The optimization mathematical model is composed of design variables, objective functions and constraints. In this article, the design variables include I_{yy} , M , V , Y , h , C_1 , C_2 , C_3 . The constraint condition is the value range of each parameter to be identified. Based on experience, the range of parameters is shown below: $I_{yy} \in [0, 0.1]$, $N \in [0, 1]$, $W \in [0, 1]$, $x \in [0, 10]$, $H \in [0, 10]$, $C_1 \in [0, 10]$, $C_2 \in [0, 10]$, $C_3 \in [0, 10]$.

IV. SYSTEM IDENTIFICATION ANALYSES

A. Comparisons and Analyses of Experimental Data

In the test process, each initial pitch angel tested 3 times, and the best data of the test data was selected as the effective data. Due to human measurement factors, there was a certain error in the test. The following figure I shows the initial pitch angle is 5 degrees, and the draft is 0.9 times the draft of design draft, design draft and 1.1 times design draft.

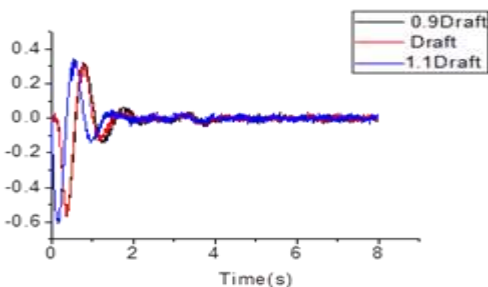


Fig. I Curves of angular velocity at initial angles of 5 degrees for different draft

As shown in figure I, when three different types of draft and initial pitch angle of 5 degrees, the peak value of the pitch angular velocity increases and the pitch period decreases with the increase of the draft, which means that the ballast increases and the sea-keeping performance increases. When the curve is near 4 seconds, the attenuation law of the curve appears an anomalous state, which may be caused by the wave disturbance caused by human factors and aggravate the pitch motion. It can be seen from the above diagram that the pitch velocity of the craft model is fast and the cycle is short, which is in line with the actual law.

B. Analyses of Identification Results

Genetic algorithm was selected to set the basic parameters as: optimization algebra was 2000, population size was 200, the probability of variable carrier was 0.01-0.0001, genetic factor was 0.1, and evolutionary weight was 0.9.

The identification and calculation of three kinds of draft and different initial pitch angles were carried out with the identification system of three different pitch mathematical models. The identification results are shown in table II.

Table II Identifying the value of the objective function of mathematical model

Objective value	function	Equation 1	Equation 2	Equation 3
1°	0.9	0.012222	0.012278	0.012231
	T	0.015295	0.015438	0.015298
	1.1	0.014992	0.015117	0.014997
2°	0.9	0.023923	0.024116	0.024039
	T	0.019096	0.019205	0.019098
	1.1	0.021258	0.021507	0.021290
3°	0.9	0.025583	0.025673	0.025583
	T	0.019560	0.019905	0.019565
	1.1	0.020014	0.020144	0.020014
4°	0.9	0.027312	0.027897	0.027589
	T	0.018670	0.020233	0.018890
	1.1	0.023269	0.023592	0.023269
5°	0.9	0.015247	0.016047	0.015246
	T	0.023616	0.024867	0.023734
	1.1	0.020237	0.020859	0.020238

By comparing the objective function values of the above three equations, it is found that the objective function value of the 5 initial pitching angles and the 3 different drafts equation 1 is the least, indicating that the fitting effect of the equation 1 is the best. Taking the design of the angle of 3 degrees below the draft as an example, the identification equation is as follows:

$$\psi_{k+1} + 8.79129395 \psi_k + 0.00850162 |\psi_k| \psi_k + 0.04839175 \psi_k^3 + 56.8982143 \psi_k^3 + 130.820453 \psi_k^2 + 32.953354 \psi_k = 0 \quad (12)$$

In order to analyze the error of the test value and the fitting value, the experimental values of the angular velocity of designed draft and the initial angle of 3 degrees were compared with the fitting values identified by formula 1, as shown in figure II.

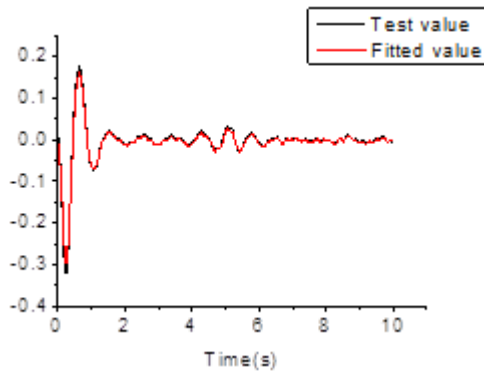


Fig. II Test angular velocity and identification angle velocity fitting curve

Table III Error table of experimental and identification results

Time (s)	Experimental angular velocity	Identification angular velocity	Error
0.60	0.124343	0.127320	2.33%
0.61	0.164479	0.161226	2.02%
0.62	0.143006	0.142625	0.27%
0.63	0.165123	0.168061	1.75%
0.64	0.170111	0.169394	0.42%
0.65	0.158781	0.159689	0.57%
0.66	0.134900	0.133365	1.15%
0.67	0.175247	0.176595	0.76%
0.68	0.158458	0.154440	2.60%
0.69	0.170776	0.169485	0.76%
0.70	0.130380	0.130956	0.44%

According to figure III, it can be seen that the fitting effect of test angular velocity and identification angular velocity is better. It can be seen from table 4.2 that the error between the test angle and the angular velocity is less than 3%, which shows that the software is reliable and can predict the angular velocity at the next moment.

C. Analyses of the hydrodynamic torque coefficient of the pitching

Through the identification and calculation of 15 groups of pitching test data, the total inertia moment of the hull, the linear damping moment coefficient, the nonlinear damping moment coefficient and the linear righting moment coefficient and the nonlinear righting moment coefficient in each case were obtained. Among them, at different initial pitch angles, the hydrodynamic moment coefficient of the craft's pitch was measured with the draft shown in figure III-IX.

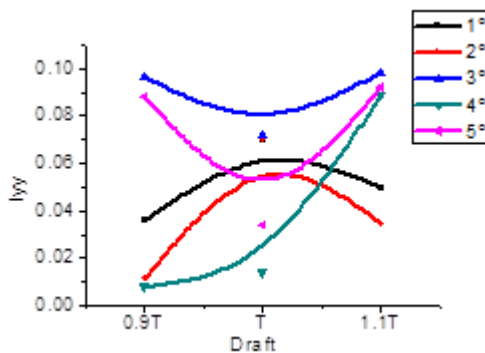


Fig. III The curves of the total moment of inertia I_{yy} of the pitch along with the initial pitch angle and draft

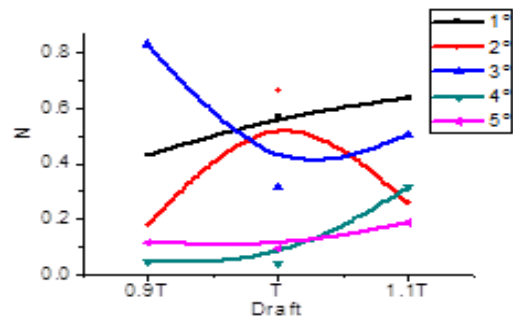


Fig. IV The curves of the linear damping coefficient N of the pitch along with the initial pitch angle and draft

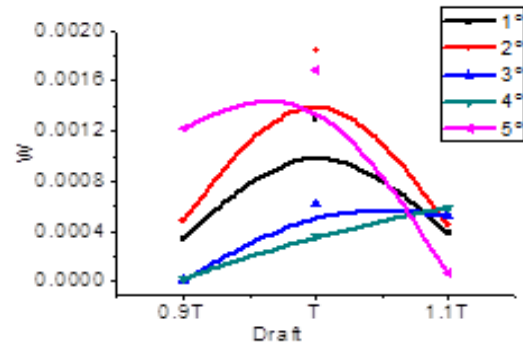


Fig. V The curves of damping moment coefficient W vary with initial pitch angle and draft

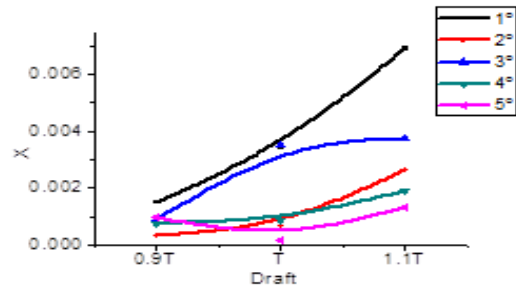


Fig. VI The curves of damping moment X vary with initial pitch angle and draft

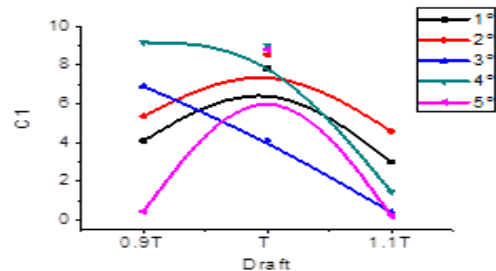


Fig. VII The curves of nonlinear righting moment coefficients C1 vary with initial pitch angle and draft

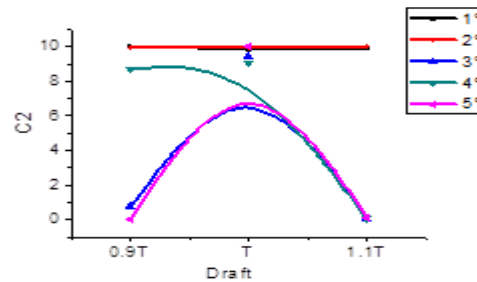


Fig. VIII The curves of nonlinear righting moment coefficients C2 vary with initial pitch angle and draft

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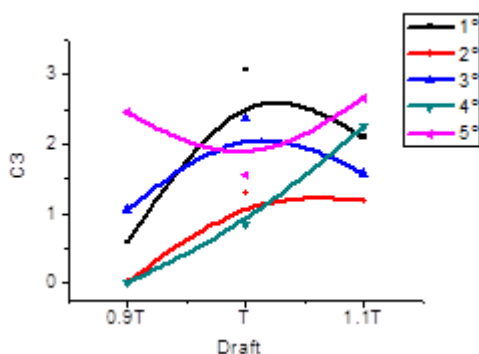


Fig. IX The curves of linear righting moment coefficient C3 with initial pitch angle and draft

It can be seen from figure IV-X that the values of the moment coefficients change with the change of draft and initial pitch angle. The total moment of inertia of the hull increases with the increase of displacement. The total moment of inertia at pitch angle 3 and 4 degrees decreases first and then increases. The linear damping moment coefficient was decreases with the increase of the initial pitch angle, but the linear damping moment coefficient was increases with the change of the draft. With the increase of initial pitch angle, the damping moment coefficient W varies little, and decreases with the increase of draft. The damping moment coefficient was increases with the increase of draft. With the increase of pitch angle, the variation of damping moment coefficient becomes smaller and smaller. The nonlinear righting moment coefficient C1 increases first and then decreases with the increase of draft. The nonlinear righting moment coefficient C1 is larger than that of draft at 3 degrees -5 degrees. The nonlinear righting moment coefficient C2 maintains a stable state with the change of draft at 1 degrees -2 degrees, and varies greatly with the change of draft at 3 degrees -5 degrees. The linear righting moment coefficient C3 increases with the increase of draft. To sum up, the nonlinear damping moment coefficient W and the nonlinear damping moment coefficient χ are smaller than the linear damping moment coefficient between 1 degree -5 degrees, indicating that the proportion of nonlinear damping is lower.

V. CONCLUSION

In this paper, the pitching motion mode of the gliding-hydrofoil craft was studied through the still water pitching test and the system identification method. Through the identification program, a mathematical model for static water pitch was found that is the most suitable for the craft model in 15 working conditions, which can accurately describe the process of the pitch motion and get the exact value of the moment coefficient. By analyzing the error of test angular velocity and identified angular velocity, the correctness of identification software was verified. Through system identification, the variation of each moment coefficient with the draft and angle of pitch was found. It shows that the system identification software can predict the future navigation parameters and movements of unmanned craft, and provide a reference for further research on the pitching motion of the gliding-hydrofoil craft.